



## Alma School Lift Station Rehabilitation

Design Concept Report September 14, 2024

City of Mesa Project No. CP0958LS01











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### 1. Introduction

The existing City of Mesa Alma School Lift Station (LS) was constructed in 1979 and rehabilitated in 2002. The site is located at 1166 W Guadalupe Road at the northeast corner of the intersection of Alma School Road and Guadalupe Road. The LS discharges to a gravity sewer approximately 50-ft west of the wet well. Figures 1 and 2 below show the site and service area respectively.

Existing LS components include:

- 30.5-ft deep, 8-ft diameter wet well
- Two submersible pumps, 1,400 gpm at 25-ft TDH each
- 8" above ground discharge piping and valves
- Natural gas emergency generator
- 18" vitrified clay pipe (VCP) gravity sewer influent line
- 10" cast iron (CI) force main
- 15" vitrified clay pipe (VCP) overflow drain pipe
- 3-ft slump block perimeter wall with steel security fence
- 16-ft wide double swing gate



**Figure 1 – Overall Site Location** 



**Figure 2 – Service Area** 

The purpose of this project is to rehabilitate the LS to replace aging components and to replace components that no longer meet City requirements. In addition, the current pump setting places the top of the pumps near the inlet sewer invert, causing wastewater to surcharge into the inlet sewer. The recent City measured wet well base elevation is approximately 4.5' higher than what is listed in the City Lift Station Inventory and what is shown on the original as-builts. Figure 3 below shows the relationship between the recent City measurements and the as-built information. In reviewing the original as-builts and the 2002 rehabilitation as-builts, it appears that the original wet well may have been filled with grout when abandoning the drywell pump configuration or when abandoning the non-standard pump configuration shown on the 2002 rehabilitation as-builts that is no longer in use. This could explain why the measured base elevation is approximately 4.5' higher than what is shown in the records and why surcharging is occurring. Pages from the original as-builts and 2002 rehabilitation as-builts B.



**Figure 3 – Wet Well Measurements** 

The City is considering two options for providing the additional wet well capacity required to eliminate the inlet sewer surcharging. Both options will eliminate the surcharging. Proposed wet cross sections, pump settings, and elevations are shown for each option on Sheet M2 of the conceptual plans in Appendix A:

- Option 1 Remove Grout & Rehabilitate Existing Wet Well
  - See Section 2 below.
- Option 2 New Wet Well
  - See Section 2 below.

### 2. Project Scope

Rehabilitation improvements will include the following:

#### LIFT STATION

- Option 1 Remove Grout & Rehabilitate Existing Wet Well
  - City to confirm grout fill depth. Confirmation of grout fill depth is not part of the DCR scope.
     GHD recommends the City obtain the services of a Job Order Contractor to set up bypass pumping, drain, clean and inspect the wet well. JOC to then Inspect bottom of wet well and perform exploratory chipping to confirm depth of grout fill and true depth of the wet well base.
  - If the JOC determines that the wet well base depth matches the original as-builts depth of 35-ft and that the grout fill can be removed, then JOC to update cost estimate for Option 1.
  - If Option 1 is deemed feasible and is still cost advantageous, GHD recommends proceeding with Option 1. In addition to the cost savings, Option 1 will have less down time and a simplified construction process compared to Option 2 due to the deep excavation required on the small site footprint for a new wet well.
  - Remove grout to wet well bottom for a pump base depth of 35-ft.
  - Inspect, repair, and recoat existing 8-ft diameter wet well.
- Option 2 New Wet Well
  - If Option 1 is no longer feasible or cost effective after the JOC inspection discussed above, then GHD recommends proceeding with Option 2.
  - Demolish existing wet well.
  - install new 8-ft diameter, 35-ft deep wet well with modified slide rail shoring excavation system.
  - Remove and replace entire existing site wall to allow for excavation.
- Replace existing precast wet well cover and hatch with safety grate. Hatch shall open toward the discharge piping.
- Replace existing MAG meter with full bore ultrasonic flow meter.
- Include "gooseneck" on the above ground discharge piping to ensure flow meter remains full.
- Hard pipe ARV drains to wet well.
- New swing check valves placed in the horizontal position.
- Replace and relocate the two ARVs to upstream of the check valves.
- Provide emergency bypass cam-lock fitting for portable pump connection.
- Replace existing rails, pump cables, and holders with heave duty 316 stainless steel.
- Replace the two existing submersible pumps and provide a third pump for the shelf.
- Provide seal around gravity overflow pipe in wet well.
- New wet well wizard set to run with either Pump 1 or 2, with the lead pump, or continuous.

#### SITE

- New decomposed granite ground cover.
- Install faux wood slats on three sides of steel fencing. Repair mortar cap on slump block wall.
- Replace existing swing gate.
- Replace the existing 1" water service with a 2" water service connection and new 2" backflow preventer located against the wall.
- Adjust site grading to remove low point from the site.
- Coat existing brick discharge manhole and concrete base.
- Rehabilitate 18" VCP gravity influent pipe with Cured-In-Place-Pipe (CIPP) based on City CCTV report dated 3/23/21
- Rehabilitate 15" VCP overflow pipe with CIPP based on City CCTV report dated 3/23/21.
- Recoat existing inlet manhole and base.
- Replace existing cast iron force main with C900 PVC pipe force main.

#### ELECTRICAL

- Replace electrical enclosure.
- Replace automatic transfer switch, pump starters, 120VAC distribution panel, PLC and cabinets.
- Replace and relocate the SES to outside of the site walls with free standing support.
- Replace wet well float switches and level transducer.
- Replace the existing generator.
- Add LED site lighting.

### 3. Design

The following sections provide the design methodology utilized to develop the conceptual design plans provided in Appendix A.

### 3.1 Submersible Pumps

The following existing site information is provided from the City Lift Station Inventory:

- Average flow = 155 gpm
- Peak flow = 310 gpm
- Pump 1 = Flygt CP3153X-415, 1400 gpm @ 25' TDH
- Pump 2 = Flygt CP3153X-415, 1400 gpm @ 25' TDH

The reported average flow matches City flow measurement data for the downstream MH3547 at approximately 153 gpm. However, the flow measurement data at MH3547 indicates that the pumps are operating at a lower flow rate of approximately 800 gpm. This is due to the pumps operating at a higher head than 25' TDH as shown on the system curve below and head loss calculations below. The MH3547 flow data is provide in Appendix C. The proposed pumps for both Option 1 and 2 will match the approximate 800 gpm flow rate per the system curve and head loss calculations below. The proposed pump data is in Appendix D.

• Flygt NP3153 MT 3 436, 15 hp, 840 gpm @ 39' TDH (Option 1 & 2)



Figure 4 – System Curve

Flow =	800											
Headloss Calculations:	Existing Cond	lition										
	Length,	Flow,	System	No. of	Equivalent	Equivalent	Velocity,					
Pipe Dia, in	ft	gal/min	Component	Comp.	Comp. Length, ft	Length, ft	ft/s	V <sup>2</sup> /2g	С	h <sub>L</sub> per 100 ft	Actual h <sub>L</sub>	Cumm. Head
8	37	800	DIP	1	37	37	5.11	0.40	130	1.18	0.44	0.4
10	53	800	DIP	1	53	53	3.27	0.17	130	0.40	0.21	0.6
8		800	90º Bend	7	20	140	5.11	0.40	130	1.18	1.66	2.3
8		800	Swing Check Valve	1	33	33	5.11	0.40	130	1.18	0.39	2.7
8		800	Plug Valve (Thru)	3	k = 0	.25	5.11	0.40	-	-	0.10	2.8
8		800	Tee Branch	1	39.9	39.9	5.11	0.40	130	1.18	0.47	3.3
8		800	Flow Meter	1	13.3	13.3	5.11	0.40	130	1.18	0.16	3.4
									1	otal Headloss (Ro	unded), ft =	3.4
										Pump Off Ele	vation, ft =	1176.0
									Elevation	of Highest Poin	t in FM, ft=	1206.6
										Stati	c Head, ft =	30.6
										TDH (Ro	unded), ft =	34.1

Flow =	840											
Headloss Calculations:		Option 1 & 2										
	Length,	Flow,	System	No. of	Equivalent	Equivalent	Velocity,					
Pipe Dia, in	ft	gal/min	Component	Comp.	Comp. Length, ft	Length, ft	ft/s	V <sup>2</sup> /2g	С	h <sub>L</sub> per 100 ft	Actual h	Cumm. Head
8	37	840	DIP	1	37	37	5.36	0.45	130	1.30	0.48	0.5
8	53	840	DIP	1	53	53	5.36	0.45	130	1.30	0.69	1.2
8		840	90º Bend	7	20	140	5.36	0.45	130	1.30	1.81	3.0
8		840	Swing Check Valve	1	33	33	5.36	0.45	130	1.30	0.43	3.4
8		840	Plug Valve (Thru)	3	k =	0.25	5.36	0.45	-	-	0.11	3.5
8		840	Tee Branch	1	39.9	39.9	5.36	0.45	130	1.30	0.52	4.0
8		840	Flow Meter	1	13.3	13.3	5.36	0.45	130	1.30	0.17	4.2
									1	Total Headloss (Rou	unded), ft =	4.2
										Pump Off Elev	/ation, ft =	1172.1
									Elevation	n of Highest Point	in FM, ft=	1206.6
										Statio	Head, ft =	34.5
										TDH (Rou	unded), ft =	38.7

#### **Table 1 – Head Loss Calculations**

### 3.2 Wet Well Sizing

The proposed pumping volume does not meet the City design requirements for minimum pumping volume (3,000 gal) per the calculations below. This is common for lift stations with low incoming

flow. The minimum volume calculation is intended to produce a retention time of 30 minutes. However, the calculation only works when the pumps are sized to match incoming flow. This is the case for larger lift stations, but small lift stations require a pumping capacity higher than the incoming flow to maintain a 4 ft/s minimum velocity. This site has an incoming flow of 155 gpm and a pumping rate of 840 gpm. The minimum pumping volume calculation only utilizes pumping capacity and does not consider the additional fill time required for low incoming flow. Using the minimum pumping volume calculation for pumping level settings at this site would result in a retention time greater than 30 minutes and excessive wet well depth. GHD recommends matching the pumping volumes proposed below and resulting retention times and pump cycles per hour:

- Minimum Pumping Volume Calculation: V = (t x q) / 4
  - V = Volume between 1<sup>st</sup> pump start level and pump stop level
  - t = minimum time between successive pump start (15 min)
  - o q = single pump capacity at the design point
  - V = (15 min x 800 gpm) / 4 = 3,000 gal (401 ft<sup>3</sup>)
- 8-ft diameter wet well cross-sectional area = 50.3 ft<sup>2</sup>
- Proposed Distance between pump on & off setting = 4.26 ft
- Proposed Pumping Volume = 4.26 ft x 50.3 ft<sup>2</sup> = 214.27 ft<sup>3</sup> (1,602 gal). The existing pump setting elevation on top of the apparent grout fill provides zero pumping volume in the wet well since the pump off setting is above the inlet invert. All existing pumping volume is coming from surcharging into the inlet sewer system. See Table 2 below for average retention time and starts per our per pump.

Data Set	Ave. Flow In (gpm)	Pumping Rate (gpm)	Pumping Volume (gal)	Fill time (min)	Pumping Duration Time (min)	Retention Time (min.)	Cycle Frequency per Hour	Starts per Hour per Pump
Option 1 & 2	155	840	1,602	10.3	2.3	12.7	4.7	2.4

**Table 2 – Retention Time & Pump Cycling** 

### 3.3 Pipe Sizing

The proposed pumping rate of 840 gpm and discharge piping size of 8" will match the existing pump and pipe sizes. The short section of existing 10" force main is oversized and can be reduced to 8". At 840 gpm, the velocity in the 8" discharge pipe and force main will be 5.4 ft/s, which meets the City's preferred requirement of 4 - 7 ft/s.

### 4. Site Improvements

### 4.1 Site Walls and Gates

#### Option 1 – Remove Grout & Rehabilitate Existing Wet Well

The mortar cap will be replaced on the 3.0' tall slump block wall. Faux wood slats will be installed on three out of four of the sides of the steel security fencing. The existing steel swing gate is out of alignment and will be replaced.

#### Option 2 – New Wet Well

The entire perimeter wall must be demolished to allow construction access required to install a modified slide rail system to excavate deep enough to remove the existing wet well, and to install the new wet well.

A new 8-ft tall CMU block wall with security pickets and 16-ft swing gate with faux wood slats will installed to replace the demolished wall.



Figure 5 – Existing Site Fence & Gate

### 4.2 Grading and Drainage

The lift station site was originally intended to drain to the adjacent retention basin located southeast of the site along with the surrounding area drainage. However, the City reported standing water within the site during rain events. GHD performed a topographic survey of the site and determined that the DG ground cover is approximately 6" lower in the center of the site than the surrounding area. Therefore, onsite drainage will pond up against the wet well and electrical pads during a rain event. The wet well cover and electrical pads are higher than the outfall of the site, so rainwater will leave the site prior to overtopping the electrical pad and wet well cover. However, the ground cover at the site should be regraded to fill in the 6" depression to eliminate the onsite ponding.

### 5. Maintenance of Plant Operation (MOPO)

Bypass pumping will be required during construction from the influent manhole, to the force main discharge manhole per figure 6 below. The bypass piping will be routed through the wall openings that were installed for bypass pumping during the previous site rehabilitation. A temporary electrical service will also be required to provide power for temporary bypass pumping since the electrical equipment will be replaced. Once bypass pumping is in place, the site can be taken out of service for construction.



**Figure 6 – Bypass Route** 

### 6. Electrical

The Alma School Lift Station is currently fed from a 200 amp, 480/277VAC, three phase service from Salt River Project. This site requires a new service entrance section to be relocated to the exterior western wall of the site. This will be fed from an existing transformer located in the SRP well site next to the lift station. It is anticipated the upgraded pump motors match the existing motors. An increase in service capacity is not anticipated.

The existing automatic transfer switch, pump starters, 120VAC distribution panel, PLC and cabinets will be replaced. The existing service entrance portion is to be removed and a new service entrance will be located outside of the site wall.

The existing 50KW generator is past its useful life and needs to be replaced. It is anticipated the new generator will be a natural gas powered 50KFW generator to match existing. This will provide adequate backup power for the entire site. All existing conduit and conductors may be reused for the generator to the ATS. Since the ATS will remain, no new signals from the ATS to the PLC are required.

The existing pumps and motors are anticipated to be replaced in kind with 15HP 480V 3 phase motors. New conductors will be installed for the new pump motors and will use most of the same conduits as existing. New conduit and conductors from the new pump motor junction boxes and the new terminal junction boxes will be required.

The existing flow meter will be replaced with a new full bore ultrasonic flow meter. The wet well level transducer will be replaced with a new ultrasonic level transducer by pulsar. New conduit and conductors for these instruments will be required.

All existing site lighting is to be replaced with new LED lights.

### 7. Opinion of Probable Cost

The preliminary Opinion of Probable Cost for both Options 1 and 2 are included in Appendix E and is summarized in Table 3 below. A 10% project contingency has been included along with a 15% market escalation factor to reflect recent market volatility and potential material and labor price increase at the time of construction.

Description	Option 1 – Remove Grout & Rehabilitate Existing Wet Well	Option 2 – New Wet Well
Materials & Labor	\$1,120,812	\$2,195,824
10% Project Contingency	\$112,081	\$219,582
15% Market Escalation Factor	\$168,122	\$329,374
15% Overhead & Profit	\$210,152	\$411,717
3% Bond & Insurance	\$42,030	\$82,343
TOTAL	\$1,653,197	\$3,238,841

### **Table 3 Preliminary Opinion of Cost Summary**

## Appendix A

## **Conceptual Plans**





Filename: G:561112577360/Digital\_Design/ACAD 2020/Figures/Sheets/Alma LS12577360-GHD-ASLS-DWG-CI-0001.dwg Plot Date: 13 September 2024 - 8:20 AM



CITY OF MESA LIFT STATION IMPROVEMENTS ALMA SCHOOL LIFT STATION

— 12" ACP W

- 12" ACP \

APN (302-87-819)

Project No. **12577360** Report No. **N/A** Date **SEPT 2024** 

**EXISTING SITE PLAN** 

C1



Filename: G:561112577360/Digital\_Design/ACAD 2020/Figures/Sheets/Alma LS12577360-GHD-ASLS-DWG-CI-0002.dwg Plot Date: 13 September 2024 - 8:21 AM



CITY OF MESA LIFT STATION IMPROVEMENTS ALMA SCHOOL LIFT STATION Project No. 12577360 Report No. N/A Date SEPT 2024

DEMOLITION PLAN



Filename: G:\561\12577360\Digital\_Design\ACAD 2020\Figures\Sheets\Alma LS\12577360-GHD-ASLS-DWG-CI-0003.dwg Plot Date: 16 September 2024 - 8:34 AM

Project No. 12577360 Report No. N/A Date SEPT 2024

C3 Source:



Filename: G\561112577360/Digital\_Design\ACAD 2020\Figures\Sheets\AIma LS\12577360-GHD-ASLS-DWG-MP-0001.dwg Plot Date: 16 September 2024 - 9:06 AM

SCALE 3/8"=1'-0" AT ORIGINAL SIZE



LIFT STATION IMPROVEMENTS ALMA SCHOOL LIFT STATION

PROPOSED LIFT STATION PLAN

Project No. **12577360** Report No. **N/A** Date **SEPT 2024** 



Filename: G\561112577360\Digital\_Design\ACAD 2020\Figures\Sheets\Alma LS\12577360-GHD-ASLS-DWG-MP-0002.dwg Plot Date: 16 September 2024 - 9:07 AM

### LEGEND

DEMOLITION AND REMOVALS







**H** | ]

CITY OF MESA LIFT STATION IMPROVEMENTS ALMA SCHOOL LIFT STATION Project No. **12577360** Report No. **N/A** Date **SEPT 2024** 

SECTIONS

M2



Filename: S\E02017 GHD Mesa Lift Stations\Alma School\DCR Alma School PID Lift Station.dwg Plot Date: 5 June 2024 - 10:34 AM

FIG E2

Appendix B

**Project As-Builts** 









2002 REHABILITATION **AS-BUILTS** A-097638

**AS-BUILT** 



DWG FILE: P:\Cad\WWMesa\22156-Alma\_School\2-sheets\C-CIVIL\C22156003.dwg Sep 13, 2002 - 10:27am OJo

PLAN SCALE: 1" = 4'-0"





BENCHMARK: BM6 N 10136.66 E10122.08 ELEVATION=1203.72 (CITY OF MESA DATUM)

SCALE: 1" = 4'-0"

#### KEYNOTE

- (1) NEW (BY-PASS) MANHOLE. SEE SECTION 1/C1.
- 2 SITE PIPING. SEE DRAWING M1
- (3) CONCRETE SLAB FOR WET WELL SHALL BE LEVEL WITH VALVES AND FLOW METER PLATFORM. SEE DETAIL C/E3
- (4) EMERGENCY POWER BACKUP GENERATOR SEE ELECTRICAL DRAWING E4
- (5) RECONNECT EXISTING GAS SERVICE LINE TO NEW GENERATOR
- 6 RETAIN AND PROTECT NATURAL GAS METER
- (7) NEW CONCRETE MCC PANEL PAD. SEE DETAIL C/E4
- (8) MAINTAIN EXISTING SITE DRAINAGE. GRADE AWAY FROM WET WELL. 3/4" MINUS DECOMPOSED GRANITE RED MOUNTAIN RED 4 INCHES THICK OVER ENTIRE SITE WITHIN ENCLOSURE WALL. APPLY PRE-EMERGENT TO ALL GRAVEL AREAS
- (9) RETAIN AND PROTECT EXISTING DISCHARGE MANHOLE. RE-SEAL LID WITH MASTIC TAPE FOLLOWING CONSTRUCTION
- (1) INSTALL EXPANSION JOINT BETWEEN VALVE SLAB AND WET WELL SLAB. SEE DETAIL F/M2

CC	CONCRETE COORDINATE TABLE									
	NORTHING	EASTING								
	10121.25	10096.91								
2	10122.30	10110.07								
3	10115.33	10110.63								
4	10097.47	10114.27								
5	10108.67	10122.20								
6	10124.62	10120.97								
$\widehat{7}$	10124.01	10112.99								

SCALE: 1" = 4'-0"

			CITY OF MESA ENGINEERING DIVISION				
BUILT	INSIDE MARICOPA COUNTY	RONALD L. ABLIN 12 ABLIN 12 ABLIN 12	ALMA SCHOOL SEWAGE LIFT STATIO	/GUADALUPE ON REHABILITATION			
		CONA, U.S.	PROPOSED				
BROW	N AND WEII	DRAWN BY: JWJ ENGINEER: APPROVED BY:	SITE IMPROVEN PLAN	MENTS C3			
		340 W.O. #3269 PROJ. NO. 02-049	SHEET 5 OF 20	CATALOG NUMBER: A-97642			



#### 2002 REHABILITATION **AS-BUILTS** A-097638

**KEYNOTES** 



SCALE: 1/2" = 1'-0"

- (1) & BALL CHECK VALVE (TYP OF 2), SEE SPECIFICATION SECTION 15120 INSTALLED HORIZON TAL INSTEAD OF VERTICAL (2) 8" ECCENTRIC PLUG VALVE (TYP OF 2), SEE SPECIFICATION SECTION 15110
- (3) 8" DIP SPOOL, LENGTH PER METER MANUFACTURER'S REQUIREMENTS
- (4) ACCESS HATCH. LOCATION AND DIMENSION SHALL BE AS RECOMMENDED BY PUMP MANUFACTURER. ACCESS HATCH SHALL BE CAST INTO LIFT STATION TOP WITH METAL FALL THROUGH PROTECTION GRATING UNDER THE ACCESS HATCH, SEE DETAIL H/M2
- (5) 8" 90° FLANGED BEND
- (6) CONCRETE EXPANSION JOINT. SEE DETAIL F/M2
- $(7) \begin{array}{c} \mbox{PROVIDE STAINLESS STEEL "KELLUM" STRAIN RELIEF SUPPORTS (TYP OF 4) \end{array} } \\ \label{eq:static}$
- (8) LEVEL SENSOR CABLE. SEE ELECTRICAL DRAWINGS
- (9) LINK SEAL (TYPICAL OF 2)
- (1) COAT ALL INTERIOR WALLS WITH PROTECTIVE COATING PER SPECIFICATION SECTION 9900
- (1) 1" SEWAGE COMBINATION AIR RELEASE VACUUM VALVE (TYP OF 2) PER DETAIL E/M2
- (12) INTERMEDIATE GUIDE BAR BRACKET PER MANUFACTURERS RECOMMENDATIONS
- (3) 2" 316 STAINLESS STEEL GUIDE BARS AS RECOMMENDED BY PUMP MANUFACTURER
- (14) POWER CABLE. CONNECT TO JUNCTION PULLBOX
- (15) CONCRETE GROUT (CLASS C). SEE SPECIFICATION SECTION 03300
- (16) 8" x 12" REDUCER WITH S.S. BOLTS
- $\overbrace{10}^{\& "}$  As mag-X flow meter as manufactured by ABB, series NO. 10DX3111E/G
- (18) 8" FLANGE COUPLING ADAPTER (TYP OF 2)
- (1) FLOAT AND POWER CABLE ACCESS J-BOX CAST IN WET WELL LID. SEE ELECTRICAL DETAIL E/E3
- (20) ULTRASONIC LEVEL SENSOR. SEE ELECTRICAL DRAWINGS
- (21) 10" 45° BEND MJ x MJ (RESTRAINED) CONNECT TO EXISTING PIPE
- (2) 8" x 8" x 8" TEE FL x FL
- (23) 10" x 8" REDUCER MJ x MJ (RESTRAINED)
- (24) PIPE SUPPORT, SEE DETAIL C/M2 (TYP)
- (25) TYPE 10 PIPE SUPPORT, SEE DETAIL A/M2 (TYP OF 4)
- (26) CONCRETE SLAB SEE DETAIL C/E3
- (27) 3" VENT WITH STAINLESS STEEL NO. 16 MESH
- B PLUG EXISTING 10" CI FORCE MAIN WITH 4000 psi CONCRETE AND ABANDON
- (29) CORE DRILL. LINK SEAL AROUND PIPE. SEE DETAIL GM/2.
- (3) 1" x 18" LONG STAINLESS STEEL ANCHOR BOLTS WITH FULL THREADED STUDS AND WASHERS. EXTEND ANCHOR INTO EXISTING CONCRETE. EPOXY ANCHOR INTO POSITION

CALL TWO WORKING DAYS BUE STAND BOTH BUE STAND CONTER 602-263-1100		CITY OF ME ENGINEERING D	SA IVISION
INSIDE MARICOPA COUNTY	RONALD L. ABUN 11	ALMA SCHOOL/GU SEWAGE LIFT STATION R	ADALUPE REHABILITATION
	CONA, U.S.	PROPOSED	DRAWING
AND	DRAWN BY: JWJ ENGINEER: APPROVED BY:	WET WELL PLAN AND SECTION	N <b>M1</b>
ע ע י	340 W.O. #3269	SHEET CATA	LOG NUMBER:

## Appendix C

### **MH3547 Flow Data**



MH3547 FLOW (mgd)

Appendix D

**Pump Data Sheets** 

### NP 3153 MT 3~ 436

Patented self cleaning semi-open channel impeller, ideal for pumping in waste water applications. Modular based design with high adaptation grade.



Curves according to: Water, pure Water, pure [100%], 39.2 °F, 62.42 lb/ft<sup>3</sup>, 1.6891E-5 ft<sup>2</sup>/s

#### Technical specification

Configuration Motor number

15hp Impeller diameter

204 mm

6 inch

N3153.185 21-15-4AA-W

**Pump information** 

Maximum operating speed

Impeller diameter 204 mm

Discharge diameter

Inlet diameter 150 mm

1755 rpm

2

40 °C

Project Block

Number of blades

Max. fluid temperature

0



$\mathbf{O}$	5,31,60	iu .				
	90 =					
	85	38%				
	75	4450%				
	70	60%5%				
	65	41740%	5%			
1 0	55		78%			
	50		78.6%			
	45		744%			
	40			70%		
TOTAL	30	76.7	%	<u> </u>	5%	
	25	11.07	$\rightarrow \times$	$\rightarrow$	60%	
	20			$\sim$		280/
	15			X	433	38% 234mm
	5				436 20	4mm
		and a second sec				
		eu				
	44					
	40					
	36					
	32					1
	28					1
	24					1
	20					1
	16					1
	12					
	8					
	4	436 204mm				1
	0 1					
	0	400 800	1200	1600	2000	[US g.p.m.]
					Curve: IS	0 9906
Installation type AA-W P - Semi permanent, Wet	Pleas	e consult your local Flyg	t representative	for performan	ce guarante	es.
Installation type AA-W P - Semi permanent, Wet Discharge diameter	Fieas	e consult your local Flyg	t representative	for performan	ce guarante	ies.
Installation type AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material	e consult your local Flyg	t representative	for performan	ce guarante	
Installation type AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
Installation type AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	
Installation type AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ies.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch speed	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	es.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion	Pieas Material Impeller Hard-Iron ™	e consult your local Flyg	t representative	for performan	ce guarante	ees.
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion ;peed re	Pieas Material Impeller Hard-Iron ™	ED Martin	t representative	for performan	ce guarante	
AA-W P - Semi permanent, Wet Discharge diameter 6 inch tion speed re	Material Impeller Hard-Iron ™	ED Martin	t representative	for performan		ies.

### NP 3153 MT 3~ 436

### Technical specification

#### Motor - General

Motor number	Phases	Rated speed	Rated power
N3153.185 21-15-4AA-W 15hp	3~	1755 rpm	15 hp
ATEX approved	Number of poles	Rated current	Stator variant
No	4	19 A	5
Frequency	Rated voltage	Insulation class	Type of Duty
60 Hz	460 V	Н	S1
Version code			
185			
Motor - Technical			
Power factor - 1/1 Load	Motor efficiency - 1/1 Load	Total moment of inertia	Starts per hour max.
0.82	87.5 %	1.61 lb ft <sup>2</sup>	30
Power factor - 3/4 Load	Motor efficiency - 3/4 Load	Starting current, direct starting	
0.77	88.5 %	114 A	
Power factor - 1/2 Load	Motor efficiency - 1/2 Load	Starting current, star-delta	
0.65	88.0 %	38 A	

GHD ENG MESA ALMA SCHOOL LS Project 0

Created by ED Martin Created on 5/21/2024 Last update

5/21/2024

FLYGT

a **xylem** brand

Block

### NP 3153 MT 3~ 436

### Dimensional drawing





Appendix E

**Opinion of Cost** 

Option 1 – Remove Grout & Rehabilitate Existing Wet Well								
Alma School Sewer Lift Station Rehabilitation								
Preliminary Opinion of	COST	Quantity	Unit Price	Total				
Description	Onit	Quantity	Omit Price	TOtal				
Construction Staking and As-Builts	LS	1	\$11,400	\$11,400				
Mobilization/De-Mobilization	LS	1	\$49,800	\$49,800				
Utility Locating	LS	1	\$21,000	\$21,000				
Demolition and Removal of Existing Piping, and Wet Well Lid/Hatch	LS	1	\$20,000	\$20,000				
Demolition and Removal of Existing Pumps	LS	1	\$6,000	\$6,000				
Demolition and Removal of Existing Steel Swing Gate	LS	1	\$3,000	\$3,000				
Demolition and Removal of SES and Generator	LS	1	\$4,500	\$4,500				
Connect to Existing Manhole	EA	1	\$6,480	\$6,480				
Faux Wood Slats	LF	102	\$100	\$10,200				
Site Grading	LS	1	\$5,000	\$5,000				
1-1/2" - 1/4" DG	SY	83	\$50	\$4,150				
16' Steel Swing Gate	EA	1	\$18,750	\$18,750				
Replace Existing Wet Well Cover and Hatch	EA	1	\$10,000	\$10,000				
Wet Well Wizard	LS	1	\$17,000	\$17,000				
Coat Existing Brick Discharge MH	SF	144	\$30	\$4,320				
Recoat Existing Inlet MH	SF	515	\$30	\$15,450				
Coat Existing 8' Diameter Wet Well	SF	1010	\$30	\$30,287				
Inspect and Repair Existing Wet Well	LS	1	\$50,000	\$50,000				
Remove Grout from Existing Wet Well	LS	1	\$20,000	\$20,000				
Submersible Pump Assembly W/ Stainless Steel Rails and Lifting Chains	EA	2	\$40,000	\$80,000				
Submersible Pump for Backup Storage	EA	1	\$30,000	\$30,000				
8" DIP Force Main	LF	102	\$310	\$31,555				
8" DIP 90 Bend	EA	3	\$2,000	\$6,000				
8" DIP Tee	EA	4	\$1,200	\$4,800				
8" Cam-Lock	EA	1	\$2,000	\$2,000				
4" x 8" DIP 90 Bend Reducer	EA	2	\$1,500	\$3,000				
8" Plug Valve	EA	3	\$2,738	\$8,213				
8" Swing Check Valve	EA	2	\$4,994	\$9,988				
8" Ultrasonic Flow Meter	EA	1	\$14,675	\$14,675				
8" PVC Force Main Piping + Fittings	LF	38	\$400	\$15,200				
New 2" Water Service	LS	1	\$5,000	\$5,000				
2" H-Tec Air Release Valve, Epoxy Coated	EA	2	\$2,625	\$5,250				
Pipe and Equipment Coating	LS	1	\$30,000	\$30,000				
Pipe Support	EA	3	\$2,600	\$7,800				
Temporary Sewer Bypass Pumping	LS	1	\$110,000	\$110,000				
CIPP ex. 18" VCP Inlet Sewer	LF	20	\$1,200	\$24,000				
CIPP ex. 15" VCP Overflow Pipe	LF	40	\$1,200	\$48,000				
Electrical Improvements & Generator	LS	1	\$377,995	\$377,995				
Subtotal				\$1,120.812				
Project Contingency	10%			\$112,081				
Market Escalation Factor	15%			\$168.122				
Overhead & Profit	15%			\$210,152				
Bond & Insurance	3%			\$42,030				
Total	370			\$1.653.197				

Option 2 – New Wet Well				
Alma School Sewer Lift Station Rehabilitation				
mesa·az Preliminary Opinion of Cost				
Description	Unit	Quantity	Unit Price	Total
Construction Staking and As-Builts	LS	1	\$11,400	\$11,400
Mobilization/De-Mobilization	LS	1	\$75,000	\$75,000
Utility Locating	LS	1	\$21,000	\$21,000
Demolition and Removal of Existing Piping	LS	1	\$20,000	\$20,000
Demolition and Removal of Existing Pumps	LS	1	\$6,000	\$6,000
Demolition and Removal of Existing Steel Swing Gate	LS	1	\$3,000	\$3,000
Demolition and Removal of SES and Generator	LS	1	\$4,500	\$4,500
Demolition and Removal of Wet Well	LS	1	\$20,000	\$20,000
Excavation & Modified Slide Rail System	LS	1	\$885,700	\$885,700
Connect to Existing Manhole	EA	1	\$6,480	\$6,480
8' Tall CMU Wall	LF	115	\$400	\$46,000
Site Grading	LS	1	\$5,000	\$5,000
1-1/2" - 1/4" DG	SY	83	\$50	\$4,150
16' Steel Swing Gate with Faux Wood Slats	EA	1	\$18,750	\$18,750
New Wet Well Cover and Hatch	EA	1	\$10,000	\$10,000
Wet Well Wizard	LS	1	\$17,000	\$17,000
Coat Existing Brick Discharge MH	SF	144	\$30	\$4,320
Recoat Existing Inlet MH	SF	515	\$30	\$15,450
New 8' Diameter 35.5 ft Deep Wet Well	FA	1	\$117 600	\$117,600
Coat New 8' Diameter Wet Well	SF	1200	\$30	\$36,000
Submersible Pump Assembly W/ Stainless Steel Rails and Lifting Cha	ns FA	2	\$40,000	\$80,000
Submersible Pump for Backup Storage	FA	1	\$30,000	\$30,000
8" DIP Force Main		102	\$310	\$31,555
8" DIP 90 Bend	E. FA	3	\$2,000	\$6,000
8" DIP Tee	FA	4	\$1,200	\$4,800
8" Cam-Lock	FA FA	1	\$2,000	\$2,000
4" x 8" DIP 90 Bend Reducer	FA	2	\$1,500	\$3,000
8" Plug Valve	FA	3	\$2,738	\$8,213
8" Swing Check Valve	FA	2	\$4,994	\$9,988
8" Ultrasonic Flow Meter	FA	1	\$14 675	\$14 675
8" PVC Force Main Piping + Fittings		38	\$400	\$15,200
New 2" Water Service		1	\$5,000	\$5,000
2" H-Tec Air Release Valve, Epoxy Coated	FA FA	2	\$2 625	\$5,250
Pipe and Equipment Coating	15	1	\$30,000	\$30,000
Pipe Support	FA	3	\$2,600	\$7,800
Temporary Sewer Bypass Pumping		1	\$165,000	\$165,000
CIPP ex_18" VCP Inlet Sewer	LG	20	\$1,200	\$24,000
CIPP ex. 15" VCP Overflow Pine		40	\$1,200	\$48,000
Electrical Improvements & Generator		1	\$377,995	\$377,995
			<i>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</i>	ψ011,000
Subtotal				\$2 105 824
Project Contingency 10%				\$210 582
Market Escalation Eactor 15%			¢220 271	
Overhead & Profit 15%			φ329,374 \$ <u>4</u> 11 717	
Rond & Insurance 20/			ψτι,/ 1/ ¢00 0/0	
			φ0∠,343 ¢2,220,044	
Total				\$3,238,841



# about GHD

GHD is one of the world's leading professional services companies operating in the global markets of water, energy and resources, environment, property and buildings, and transportation. We provide engineering, environmental, and construction services to private and public sector clients.

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